ARIZONA NUMERICAL RANKING SYSTEM FOR JURISDICTIONAL DAMS WITH SAFETY DEFICIENCIES

1.0 Introduction

The Arizona Department of Water Resources (ADWR), Dam Safety Section, has a responsibility to protect human life and property from the improper operation or failure of a dam. The Department supervises the safety of over 200 dams in Arizona with limited staff and resources. There is a need for a method of prioritizing dams within its inventory of jurisdictional dams for several purposes including, distribution of loan or grant money to repair dams, internal budgeting, and enforcement action. For this reason, Tetra Tech Inc. and Arizona State University have developed a numerical ranking or prioritizing system for the dams with safety deficiencies within the Department's inventory of dams. Documentation of the development of the system and selected references are included as Appendices in the Tetra Tech, Inc. report titled "Numerical Ranking System for Jurisdictional Dams In Arizona," dated July 2001.

2.0 Process Description

This prioritization-ranking system, modeled after a similar system used by the State of Washington, provides a scoring of dams with safety deficiencies within State jurisdiction based on a consequences of failure category described by the number of persons at risk (PAR) and the number and severity of deficiencies related to typical failure modes. Currently, only dams with High or Significant Hazard Potential Classifications are considered to have safety deficiencies. Very Low and Low Hazard Potential Classifications are excluded because potential economic, lifeline, and intangible losses are low or restricted to the dam owner's property. Five categories of potential failure modes have been delineated. These include: 1) Hydrologic Adequacy, 2) Potential for Piping, 3) Dam Stability, 4) Condition of Outlet Works, and 5) Unique Conditions. A scale ranging from "Satisfactory" to "Severe" describes the seriousness of each identified deficiency. Use of the term "Severe" instead of "Emergency" is a deviation from Washington State terminology for clarification purposes. A true emergency situation falls out of the realm of this ranking scheme, as it requires immediate mitigative action.

The six categories (i.e. PAR and five potential failure modes) constitute a method of simplifying a more complex reality. The scoring gives a relative ranking of one dam to another. This is not an absolute score, nor is it unchanging. The process is a dynamic one. Ultimately, the final ranking of seriousness at a particular time must be confirmed based on the knowledge and judgment of engineers experienced in dam technology as well as additional detailed studies, when deemed appropriate.

The first step in the process of scoring a dam is to gather the available significant information regarding the dam. The information is reviewed and the number of persons at risk as well as the conditions at the dam are summarized on the Basic Information Summary Work Sheet (pages 7 & 8). This step, performed by a qualified engineer experienced in dam technology, is completed prior to any scoring of the dam. A USGS quadrangle map showing the dam is desirable. The most recent inspection report, the most recent safety deficiency letter, and executive summaries or other significant information from previous studies and/or Phase I type inspections should also

be reviewed and listed on the Basic Information Summary Work Sheet as references. This information documents the considerations incorporated into the scoring and ranking.

The second step is to compare the information from the files compiled on the Basic Information Summary Work Sheet with the Scoring Descriptions for Category I (Page 9) as well as Categories II.A. – II.E. (Pages 10 – 17) and to assign (score) points in accordance with these descriptions. The categories are described in more detail in the following section. The conditions described in the Category II scoring descriptions are presented as guidelines. Deficiencies, which are not explicitly described in the scoring descriptions, should be assigned points in a manner consistent with the seriousness relative to those conditions described. For those dams where a deficiency is suspected but its seriousness is unknown, points should be awarded based on engineering judgment in the category of concern until further evaluation is possible. A Scoring Summary Work Sheet is provided to allow a gathering of the scores for the dam onto one sheet (Page 18).

The worst-case condition for each category dictates the score and only one score can be given to each category. Some safety deficiencies could be described by more than one category. In these instances, points should be allotted in one category only, so as to not double-count the deficiency. Once each category has been scored, a total score for the dam is calculated.

Total ranking points for each dam are determined by adding the PAR points to the potential failure mode deficiency points on the Scoring Summary Work Sheet. In recognition of the fact that the risk associated with a single "Major" or "Severe" deficiency is much higher than that associated with the summation of numerous "Minor" or "Moderate" deficiencies, the final point total is divided in half when no deficiency category exceeds the "Minor" or "Moderate" level.

The deficiency categorizations and point allocations contained within this ranking system were developed for the narrow purpose of developing relative rankings of dams with safety deficiencies. The system gives higher priority to the repair of dams in immediate distress versus those with deficiencies related to the occurrence of extreme events (i.e. large floods and earthquakes). The numerical point totals are not intended to represent the absolute levels of hazard or risk associated with each dam and should not be used as criteria for establishment of Unsafe Dam classifications.

Given the inherent uncertainty in the information used and the repeatability of the application of the category descriptions, point totals differing by less than a moderate deficiency (i.e. 65 points) may be considered equivalent. After an initial ranking identifies a group of similarly scored dams near the top, more detailed studies and subsequent re-ranking of just these dams can be used for refinement of the rankings. In any event, the numerical ranking is used as a starting point, after which additional studies or other project specific non-technical intangibles may be incorporated into the decision making process.

3.0 Category Descriptions

The category descriptions are provided below to give guidance and consistency to those scoring the dams. Some explanatory comments on the descriptions are also included.

3.1 Section I – Consequences of Failure

Category I. Persons at Risk (See Page 9)

In as much as loss of life is the single most important consequence of a dam failure, Persons at Risk (PAR) is used as the surrogate measure of consequence in this system. PAR is the number of people, who without evacuation, are within the area of an inundation flood of certain defined criteria of depth and/or velocity due to dam failure during the Inflow Design Flood (IDF) including discharges from the outlets and spillways. The Bureau of Reclamation has published detailed information on the hazards posed by various combinations of floodwater depth and velocity in their 1988 document *Downstream Hazard Classification Guidelines, ACER Technical Memorandum No. 11.* Based on this information, the Arizona Ranking System establishes criteria of a depth of greater than one foot and/or a velocity greater than two feet per second for defining the inundation area.

It is commonly assumed that each permanent dwelling has three occupants. Site-specific information about the likely occupancy should be used at worksites and temporary use facilities such as resorts, campsites, and recreational areas. Those situations where PAR is not an adequate measure of the consequences of a failure can be adjusted as a unique condition (See Category II.E.).

Not all dams have had a dam break analysis performed at this time. Remember that for this scoring, the lines of demarcation may be such that it is very clear which category applies. In the event that a question exists, one of several simple methods may be applied. These are described in Preliminary Safety Evaluation of Existing Dams, prepared for FEMA by Stanford University, December 1984. The Simplified Dam Break program (NWS) is probably the most used of the methods.

3.2 Section II – Potential Failure Modes and Seriousness of Deficiencies

3.2.1 Category II.A. Hydrologic Adequacy (See Page 10)

Hydrologic adequacy is measured in terms of the size of the flood, as a percentage of the Probable Maximum Flood (PMF), which results in an overtopping depth greater than the defined critical value. In the absence of site-specific information regarding the critical depth of overtopping, simplified estimates based on the type and condition of the dam are provided. These estimates are adopted from information presented in the 1983 Stanford/FEMA document, *Preliminary Safety Evaluation of Existing Dams*, and the 1997 Bureau of Reclamation Risk Based Profile System. The severity of the safety deficiency is related to the magnitude of the IDF of the dam under consideration. Arizona Rules for Dam Safety prescribe the magnitude of the IDF to vary with size and hazard classification. Arizona Rules for Dam Safety do not specifically define the IDF for high hazard potential dams. The Rule states, "For a high hazard potential dam, the applicant shall design the dam to withstand an inflow design flood that varies from .5 PMF to the full PMF, with size increasing based on persons at risk and potential for downstream damage. The applicant shall consider foreseeable future conditions." (AAC 12.15.1216. A. 2.) ADWR criteria for High Hazard Dams are thus established as follows:

In accordance with A.A.C. R12-15-1216 (A)(2), the inflow design flood (IDF) for high hazard potential dams shall be the full probable maximum flood (PMF) if the persons at risk (PAR) is more than 300; the IDF shall be 0.75 PMF if the PAR is between 31 and 300; and the IDF shall be 0.5 PMF if the PAR is less than 31. The IDF shall be increased from 0.5 PMF or 0.75 PMF if there is a high potential for extensive downstream damage and/or severe disruption of critical lifeline services.

The IDF criteria for High Hazard Potential Dams was developed based on the results of a review of the criteria used by other agencies. Supporting documentation is presented in Appendix B.

3.2.2 Category II.B. Potential for Embankment or Foundation Piping (See Page 11)

This category description is intended to address all issues relating to the potential for piping failures in embankment dams and/or in foundations. It includes cracks or other potential flow paths that may exist or be developing through or under a dam. Cracking of embankments or concrete, animal burrows, detrimental vegetation, flows along poor construction joints, poor abutment contacts, and flow paths along any penetrations through the dam should all be considered.

Appropriate filter design is important to resist piping and is an important consideration. In general, dams designed prior to 1960 did not include filters. Dams constructed between 1960 and 1985 may have filters that do not meet current standards. The current standards were developed though testing in the early 1980's. Arizona Dam Safety Rules require "The design of any significant or high hazard potential dam shall provide seepage collection and prevent internal erosion or piping due to embankment cracking or other causes." (AAC 12.15.1216. B. 3.)

Studies by Leonards, and Narain indicate that embankment dams constructed of silt or silty sand material are more susceptible to cracking. (Leonards, and Narain, "Flexibility of clay and cracking of earth dams," ASCE SM 2 March 1963)

3.2.3 Category II.C. Dam Stability (See Pages 12 – 15)

This category includes three description sections, the Embankment Dam Static Stability section, the Concrete and Masonry Dam Static Stability section, and the Seismic Stability section. As with all categories, the worst-case stability condition (i.e. static or seismic) governs the score assigned for the overall category.

The Embankment Dam Static Stability section describes the factors that relate to the stability of an embankment dam under static loading conditions. In those cases where no stability calculations are available, a first cut analysis can be made by comparing the dam with the suggested safe slopes found in the USBR Design of Small Dams, 1987 (Figures 6.5 and 6.6), included on Page 13.

If the dam is a concrete or masonry dam, the <u>Concrete and Masonry Dam Static Stability</u> section addresses the issues that would be considered <u>instead of</u> those listed in the Embankment Dam Static Stability section.

The <u>Seismic Stability</u> section addresses seismic stability for <u>all dams</u>. The deficiency categories are each divided into three subcategories; (1) A seismic stability analysis has been performed, (2) An embankment dam for which no analysis has been performed, and (3) A concrete or masonry dam for which no analysis has been performed. In order to lend higher priority to the repair of dams in immediate distress versus those with deficiencies related to the occurrence of earthquake events, the "Major" and "Severe" deficiency categories are reserved for static loadings only.

In the absence of a site-specific study, a preliminary evaluation of seismic risk is made using the "Map of Horizontal Acceleration at Bedrock for Arizona with 90 Percent Probability of Non-Exceedance in 250 Years," by Euge, K. M., Schell, B. A., and Lam I. P., 1992, developed as part of an Arizona Department of Transportation sponsored research study. The acceleration values associated with this map have a return period of about 2500 years.

3.2.4 Category II.D. Condition of Outlet Conduit (See Page 16)

The category descriptions and conditions are adapted from a paper presented at the 1989 ASDSO Annual Conference, titled, "Evaluation of the Condition of Principal Spillway Conduits," written by Koeliker, Lin and Best. The evaluation described in the paper is based on observations made within each outlet with a camera. In the event that such photographs are not available at the time of the scoring, engineering judgment must be applied based on all other observations that are available.

Ranking points allocated in this category relate only to the physical condition of the outlet conduit. In the event of seepage occurring along the outside of the conduit, points should be allocated in *Potential for Embankment or Foundation Piping Category* as is the case for uncontrolled seepage along any penetration.

3.2.5 Category II.E. Unique Conditions (See Page 17)

Unique conditions should be only those conditions that cannot be incorporated within one of the other categories. The word "Unique" has the following synonyms: only one of its kind, sole, exclusive, exceptional, distinctive, and rare. This category gives the person scoring the dam an opportunity to add points for some of these situations or conditions.

The following examples are conditions that may be considered unique:

- Potential landslides or other deficiencies within the reservoir boundaries,
- Regional or local ground subsidence,
- Inadequate outlet discharge capacity,
- Spillway flow passing over or encroaching on dam,
- Vandalism.
- Downstream valve control in an embankment dam,
- Potential extreme lifeline losses, or
- Irreplaceable intangible losses.

Ranking points should be applied based on seriousness of the deficiency in a manner consistent with points allocated in other categories. Examples of possible unique conditions and recommended ranges of points are provided for assistance.

4.0 Point Tabulation

Total Ranking Points are determined for each dam by adding the Consequences of Failure (PAR) points to the Potential Failure Modes Deficiency points on the Scoring Summary Work Sheet as shown below.

Section I. Consequences of Failure

Category I	Persons at Risk	Points
Section II. Potential Failure Modes and	Seriousness of Deficiencies	
Category II.A.	Hydrologic Adequacy	Points
Category II.B.	Potential for Piping	Points
Category II.C.	Dam Stability	Points
Category II.D.	Outlet Conduit	Points
Category II.E.	Unique Conditions	Points
	_	Total Points

In the event that none of the identified deficiencies exceed the level of "Minor" or "Moderate," the final point total is multiplied by a factor of 0.5.

5.0 Attachments

- 1. Ranking of Dams, Basic Information Summary Worksheet (Two pages)
- 2. Ranking of Dams, Category Scoring Descriptions (Nine pages)
- 3. Ranking of Dams, Scoring Summary Worksheet (One page)

RANKING OF DAMS BASIC INFORMATION SUMMARY WORK SHEET (1of 2)

(Enter data from files and other information available on the dam.)

Dam Name	ID no.	Date	Engineer	
Date last inspected:	(Attach report	t) Hazard Potent	tial Class: (circle)	H S
Type: Safet	y status: (circle) Unsa	afe Safety Deficie	ency Satisfacto	ory
Height:(ft) Storage Ca	pacity:	(ac. ft.) Size Class (ci	rcle) S	I L
Year Completed	Latitude:	Longitude:	Drainage Are	:a:
Downstream Community:	Dist	(mi)		
Section I. CONSEQUE	NSES OF FAILURE			
Category I. Persons at R	isk (PAR)			
PAR is the number of people, w greater than one foot and/or a ve Flood (IDF) including discharge worksites, and temporary use ar The only delineation necessary (d) more than 300 PAR. If an inundation study has been engineering firm performing the approximate method. In many of	elocity greater than two es from the conduits an eas. is between (a) Zero PA completed, use the info e study. If no study has	o feet per second due to d spillways. PAR incl a.R, (b) 1 to 3 PAR, (b) ormation provided and s been completed use s	o dam failure during the udes persons at perma of 4 to 30 PAR, (c) 31 to list study date and the implified dam break of	ne Inflow Design ment dwellings, to 300 PAR, and experson or r some other
<u>Circle one :</u>				
0 PAR 1 – 3 P	AR 4 – 30 PAR	31 – 300 PAR	More than 300	PAR
Comments:				
<u>List studies:</u>				
Section II. POTENTIAL FAIL (Use inspection reports and studi				

Category II.A. Hydrologic Adequacy Inflow Design Flood (IDF):

Describe present spillway capacity in percent of PMF if available:

Other information on the spillway:

RANKING OF DAMS BASIC INFORMATION SUMMARY WORK SHEET (2of 2)

(Enter data from files and other information available on the dam.)

Dam Name	ID no.	Date	Engineer
	for Piping Failure Describe	quantity of seepage.	. Is it consistent with design?
Is piping evident?			
Category II.C. Dam Stal			
	ge Factors of Safety: ool) and do	wnstream (full po	ol)
oponomii (pinimi p	and do	wasaraan (ran po	··,
Seismic: Peak Grou	and Acceleration (PGA) from	ADOT Map =	% of g.
		•	-
Category II.D. Outlet Co and joints, etc.)	nduit (Describe construction	n method, seepage	e protection, cracking, corrosion, lining
and joints, etc.)			
Category II F — Unique C	onditions (Describe all condi	tions qualifying a	as sole, exceptional, only one of its kind,
distinctive, and/or i	rare. Such conditions do not f	it into any other c	ategory but may have significant impact
on the potential for	failure or damage downstream	m in the event of	a failure.)

CATEGORY I. PERSONS AT RISK (PAR)

PAR is the number of people, who without evacuation, are within the area of an inundation flood of a depth of greater than one foot and/or a velocity greater than two feet per second due to dam failure during the Inflow Design Flood (IDF) including discharges from the conduits and spillways. PAR includes persons at permanent dwellings, worksites, and temporary use areas.

It is commonly assumed that each permanent dwelling has 3 occupants. Site-specific information about the likely occupancy should be used at worksites and temporary use facilities such as resorts, campsites, and recreational areas.

	Description
0 points	Zero persons at risk
200 points	1 to 3 persons at risk
300 points	4 to 30 persons at risk
400 points	31 to 300 persons at risk
500 points	More than 300 persons at risk

CATEGORY II.A. HYDROLOGIC ADEQUACY

Matrix for Evaluating Seriousness of Dam Deficiencies

(The worst condition governs in the overall rating for Category II.A.)

Step 1: Estimate the critical overtopping depth, d_c, for the dam under consideration.

Type of Dam	Condition	d _c [ft]
Concrete	Good Condition – Very little seepage	(Height) ^{0.6}
Gravity	No crack or movement	
	Fair Condition – Moderate seepage	$(\text{Height})^{0.45} - 1$
	Small structural cracks	_
	Slight differential movement	
	Poor Condition – Excessive seepage	$(\text{Height})^{0.3} - 2$
	Large continuous cracks	
	Excessive differential movement	
	Poor foundation condition, i.e. especially vulnerable to	Zero
	overtopping	
Thin Arch or	See Concrete Gravity	Value calculated for Gravity
Buttress		Dam divided by two
Embankment	Inadequate erosion protection	Zero
	Erosion protection	1

Note: Based on Preliminary Safety Evaluation of Existing Dams, Stanford/FEMA, 1983, and the 1997 Bureau of Reclamation Risk Based Profile System.

- Step 2: Determine the percentage of the PMF required to cause an overtopping depth, d_o , which exceeds the d_c estimated in Step 1.
- Step 3: <u>IDF is greater than or equal to 0.5 PMF:</u> Compare the percentage of the PMF obtained in Step 2 to the ranges provided in the table below for the appropriate IDF and allocate the points shown.

<u>IDF</u> is 0.25 <u>PMF</u>: If the percentage of the PMF obtained in Step 2 is less than 25 then allocate 145 points.

	IDF			
	0.5 PMF 0.75 PMF PMF			
Satisfactory O points	More than 50% of PMF	More than 75% of PMF	More than 100% of PMF	
0 points				
Minor	45% to 50% of PMF	63% to 75% of PMF	80% to 100% of PMF.	
20 points				
Moderate 65 points	40% to 44% of PMF	50% to 62% of PMF	60% to 79% of PMF	
Major	25% to 39% of PMF	25% to 49% of PMF	25% to 59% of PMF	
145 points	Or, spillway channel or control is highly eroded.			
Severe 300 points	Less than 25% of the PMF. Or, spillway is highly erodible and likely to result in sudden release of reservoir.			

Step 4: If the spillway is highly eroded or likely to fail structurally, then allocate points as described in the above table if they are greater than the points that result from Step 3.

CATEGORY II.B. EMBANKMENT and FOUNDATION PIPING

Matrix for Evaluating Seriousness of Dam Deficiencies

(The worst condition governs in the overall rating for Category II.B.)

Satisfactory	No signs of defects or distress of embankment or foundation.
0 points	Seepage is in agreement with design expectations. Adequate filter drain system (including conduit filter diaphragm) exists.
o points	No trees or deep-rooted vegetation on the embankment or within toe area.
Minor	Evidence of minor defects, such as burrow holes and/or localized
	deep-rooted vegetation.
20 points	Minor uncontrolled clear seepage and no evidence of internal erosion. Embankment constructed with fine silty sand or non-dispersive clayey silt material. Filter drain system adequacy unknown.
Moderate	Numerous shallow (< 2 feet deep) burrow holes and/or cracks on one or both slopes and/or crest of embankment.
65 points	Shallow-rooted trees less than 6 feet tall and less than 4 inches in diameter on the embankment or within toe area.
	Embankment constructed on unconsolidated alluvial, limestone, or gravel foundation without cutoff or key.
	Embankment filter drain system (including conduit filter diaphragm) is nonexistent or inadequate.
	Geotextiles used a sole defense against dam failure.
	Evidence of poor embankment compaction or poor or inadequate bond to foundation and abutments.
	Moderate uncontrolled clear seepage and no evidence of internal erosion.
Major	Embankment, foundations, or abutments with large or deep-rooted trees, isolated deep sinkholes and/or animal borrows.
145 points	Extensive hairline transverse embankment cracking (< 2 feet deep) in absence of adequate filter drain.
	Significant uncontrolled clear seepage and no evidence of internal erosion.
	Significant differential settlement of portions of the embankment.
Severe	Embankment, foundations, or and abutments with extensive open cracks
200	$(\geq \frac{1}{4}$ " wide and > 2 feet deep), numerous deep sink holes and/or
300 points	large-animal borrows.
	Significant concern for or evidence of piping (i.e. internal erosion) and/or sand boils. Abrupt changes in seepage.
	Subsidence crack through embankment or abutment.

CATEGORY II.C. DAM STABILITY 1. EMBANKMENT DAMS (STATIC STABILITY)

Matrix for Evaluating Seriousness of Dam Deficiencies

(The worst condition governs in the overall rating for Category II.C.)

	Description
Satisfactory	No signs of defects or distress of embankment or foundation.
	Movement is in agreement with design expectations.
0 points	Pore pressures, if known, are consistent with design.
Minor	Some evidence of minor defects, such as minor erosion of the slopes.
20	Embankment constructed with silt or sandy silt material.
20 points	
Moderate	Numerous shallow (less than 2 feet deep) erosion gullies on one or both slopes and/or crest of embankment.
65 points	Embankment constructed on unconsolidated alluvial foundation.
	Evidence of poor embankment compaction or poor or inadequate bond to
	foundation and abutments, which may lead to embankment movement.
	1.3 ≤ Computed Factor of Safety < 1.5 [Steady state seepage: upstream (partial pool) and downstream (full pool)].
	If no FS has been computed, D/S slopes are steeper than prescribed by Table 6.5
	or Table 6.6, Design of Small Dams, USBR 1987 (Tables included on next page).
Major	Distressed embankment, foundations, or abutments.
145 points	1.0 ≤ Computed Factor of Safety < 1.3 [Steady state seepage - Upstream (partial pool) and downstream (full pool)].
145 points	Evidence of pore pressures significantly higher than design values.
	Evidence of pore pressures significantly higher than design values.
Severe	Unusual and sudden change in pore pressure information.
	Misalignment, sloughing or bulging of embankment.
300 points	Evidence of heave on downstream slope.
	Tilting of the crest, deep longitudinal tension cracks.
	Movement of the outlet conduit.
	Computed Factor of Safety < 1.0 [Steady state seepage - Upstream (partial pool) and
	downstream (full pool)].
-	

Table $6.5~\mathrm{from}$ Design of Small Dams, USBR 1987

(For Homogeneous Dams on stable foundation*)

Case	Туре	Purpose	Subject to rapid drawdown	Soil class	Upstream Slope - No steeper than:	Downstream Slope - No steeper than:
				GW, GP, SW, SP	Pervious	Unsuitable
A	Homogeneous	Detention or		GC, GM, SC, SM	2.5:1	2:1
	or modified	Storage	No	CL, ML	3:1	2.5:1
	Homogeneous			CH, MH	3.5:1	2.5:1
				GW, GP, SW, SP	Pervious	Unsuitable
В	Modified	Storage	Yes	GC, GM, SC, SM	3:1	2:1
	Homogeneous			CL, ML	3.5:1	2.5:1
				CH, MH	4:1	2.5:1

^{*}Dams constructed on soft foundations require special consideration

Table 6.6 from Design of Small Dams, USBR 1987 (For Zoned Dams on stable foundation*)

Туре	Purpose	Subject to rapid drawdown	Shell Material Classification	Core Material Classification	Upstream Slope - No steeper than:	Downstream Slope - No steeper than:
Zoned with minimum core A	Any	Not critical	Rockfill, GW,GP, SW (Gravelly) SP (Gravelly)	GC, GM, SC, SM, CL, ML, CH, MH	2:1	2:1
Zoned with Maximum Core	Detention or Storage	No	Rockfill, GW,GP, SW (Gravelly) SP (Gravelly)	GC, GM, SC, SM, CL, ML, CH, MH	2:1 2.25:1 2.5:1 3:1	2:1 2.25:1 2.5:1 3:1
Zoned with Maximum Core	Storage	Yes	Rockfill, GW,GP, SW (Gravelly) SP (Gravelly)	GC, GM, SC, SM, CL, ML, CH, MH	2.5:1 2.5:1 3:1 3.5:1	2:1 2.25:1 2.5:1 3:1

^{*}Dams constructed on soft foundations require special consideration

CATEGORY II.C. DAM STABILITY 2. CONCRETE or MASONRY DAMS (STATIC STABILITY)

Matrix for Evaluating Seriousness of Deficiencies

(The worst condition governs in the overall rating for Category II.C.)

Satisfactory Good condition, only minor or no unusual cracking, spalling, scaling pop-outs or movements observed but not considered to be of structural significance. Minor Only minor seepage. Seepage is clear, measured and not increasing over time. Dam has no system for monitoring movement. Design strength of concrete unknown. Design information unavailable. Seepage is unmeasured and clear. Very small structural cracks that appear to be localized about highly stressed areas (such as abutments). Localized surficial weakness of structural concrete due to degradation, spalling, or alkali aggregate reaction. Major* Extensive evidence of concrete weakness due to degradation, spalling, or
Minor Only minor seepage. Seepage is clear, measured and not increasing over time. Dam has no system for monitoring movement. Moderate Design strength of concrete unknown. Design information unavailable. Seepage is unmeasured and clear. Very small structural cracks that appear to be localized about highly stressed areas (such as abutments). Localized surficial weakness of structural concrete due to degradation, spalling, or alkali aggregate reaction. Major* Extensive evidence of concrete weakness due to degradation, spalling, or
Minor Only minor seepage. Seepage is clear, measured and not increasing over time. Dam has no system for monitoring movement. Moderate Design strength of concrete unknown. Design information unavailable. Seepage is unmeasured and clear. Very small structural cracks that appear to be localized about highly stressed areas (such as abutments). Localized surficial weakness of structural concrete due to degradation, spalling, or alkali aggregate reaction. Major* Extensive evidence of concrete weakness due to degradation, spalling, or
20 points Moderate Design strength of concrete unknown. Design information unavailable. Seepage is unmeasured and clear. Very small structural cracks that appear to be localized about highly stressed areas (such as abutments). Localized surficial weakness of structural concrete due to degradation, spalling, or alkali aggregate reaction. Major* Extensive evidence of concrete weakness due to degradation, spalling, or
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or alkali aggregate reaction. Major* Extensive evidence of concrete weakness due to degradation, spalling, or
Major* Extensive evidence of concrete weakness due to degradation, spalling, or
all-ali a serre seta manetica
alkali aggregate reaction.
Binding of gates and valves and/or deformations in conduits or interior access tunnels. Evidence of structural cracking.
Insitu strength unknown or questionable.
Heavy seepage from lift lines, abutments or cracks. Seepage may carry fines.
Abutment distress or instability (e.g. rockfall) in case of arch dams.
Severe* Deformation and/or differential movements greater than anticipated in design.
Large continuous structural cracks.
300 points Localized crushing, bending or buckling of concrete.
Opening of construction joints.
Excessive or increasing seepage at lift lines, abutments or cracks.
Severe scaling, large pop-outs, and spalling.

^{*}A closer structural examination may be required for delineation between "Major" and "Severe" deficiency ratings.

CATEGORY II.C. DAM STABILITY 3. ALL DAM TYPES (SEISMIC STABILITY)

Matrix for Evaluating Seriousness of Deficiencies

(The worst condition governs in the overall rating for Category II.C.)

Description

Satisfactory 0 points	Analysis indicates adequate seismic stability under design load, liquefaction of embankment and foundation unlikely.
v points	If no analysis, embankment well compacted, dam founded on stable foundation and/or Peak Ground Acceleration $PGA \le 0.15g$.
	If no analysis, concrete or masonry dams with PGA \leq 0.2g.
Minor	Analysis indicates marginal seismic stability and/or deformation results in loss of
20 points	freeboard (D ≤ freeboard) and/or isolated limited zones of liquefaction of embankment or foundation under design load.
	If no analysis, saturated alluvial foundation or embankment is not well compacted and PGA > 0.15g.
	If no analysis, concrete or masonry dams with $0.2g < PGA \le 0.25g$.
Moderate ²	Analysis indicates inadequate seismic stability, excessive deformation (D > freeboard) and/or widespread liquefaction of embankment or foundation under design load.
65 points	
	If no analysis, loose, saturated alluvial foundation or embankment with high pore pressures is not well compacted and PGA > 0.15g.
	If no analysis, concrete or masonry dam with PGA > 0.25g.

Note¹: Peak Ground Acceleration (PGA) obtained from site-specific studies or "Map of Horizontal Acceleration at Bedrock for Arizona with 90 Percent Probability of Non-Exceedance in 250 Years," by Lam I. P., Schell, B. A., and Euge, K. M., 1992, ADOT Report No. AZ92-344.

Note²: In order to give higher priority to the repair of dams in immediate distress versus those with deficiencies related to the occurrence of earthquake events, the "Major" and "Severe" CATEGORY II.C. deficiency delineations are reserved for static loadings only.

CATEGORY II.D. OUTLET CONDUIT

Matrix for Evaluating Seriousness of Deficiencies

(The worst condition governs in the overall rating for Category II.D.)

	RATING ¹	CRACKS	CORROSION	LINING	JOINTS
Satisfactory	9	None; new condition	None; new condition	No loss, new condition	Watertight; gaps well within tolerance
0 Points	8	If any they are hairline and of no structural concern	Very little	Slight evidence of abrasion, scouring, cracking or spalling	No evidence of seepage at any joint; gaps within tolerance
Minor	7	Minor and free of leaks or evidence of leakage	Minor, no obvious loss of material evident	Minor evidence of abrasion, scouring, cracking, or spalling	One or more show signs of minor leakage; gaps within
20 points					tolerance
Moderate ² 65 points	6	Less than 1/8" and show only minor evidence of leakage	Some deterioration of material evident	Some loss to the point that underlying material is exposed at several locations	One or more have signs of leakage and/or deterioration; gaps within tolerance
os points	5	Less than 1/4" and show evidence of leakage	Significant deterioration at one or more locations evident	Missing on parts of the conduit through the length	One or more show evidence of leakage and/or deterioration; gaps within tolerance
Major	4	Large enough to show considerable evidence of leakage	Deterioration to point of concern for long-term structural integrity of conduit	Loss so substantial that there is concern for the durability of the underlying material	One or more is leaking and/or significantly deteriorated; gap exceeds tolerance
145 points	3	Openings large enough to affect the integrity of the embankment	Corroded to the point of leakage expected at one or more locations	No longer effective throughout the conduit	Leak large enough to affect embankment; gap well beyond tolerance
Severe	2	Embankment is being affected by allowing erosion of the	Corroded so much that leaks are evident	Completely missing	Embankment exposed at one or more joints; alignment of
300 points		embankment			sections affected
	1	Flow occurring outside the conduit as well as inside	Corrosion so substantial that structural integrity of conduit is in question		Water freely flowing though joints as freely as in the conduit; ends no longer line up
	0	Conduit no longer main path of flow because of losses through cracks	So much material lost to corrosion that conduit is no longer capable or supporting the fill		

Note¹. KSU Ratings for Conduits from Table 1 of "Evaluation of the Condition of Principal Spillway Conduits," Koelliker, et al. 1989, ASDSO Conf. Note²: The presence of a corrugated metal pipe (CMP) outlet is treated as a Moderate Deficiency.

CATEGORY II.E. UNIQUE CONDITIONS

Matrix for Evaluating Seriousness of Deficiencies

(The worst condition governs in the overall rating for Category II.E.)

A unique condition must qualify as sole, exceptional, only one of its kind, distinctive, and/or rare. Such conditions do not fit into any other category but may have significant impact on the potential for failure or damage downstream in the event of a failure.

Ranking points should be applied based on seriousness of the deficiency in a manner consistent with points allocated in other categories. Examples of possible unique conditions and recommended ranges of points are provided below.

	R	ecommended P	oint Assignmer	nts
Example of Possible Unique Conditions	Minor 20 points	Moderate 65 points	Major 145 points	Severe 300 points
Vandalism of outlet works occurs regularly	X	X		
Reservoir rim has active landslide with significant volume compared to reservoir volume			X	X
Inadequate outlet discharge capacity to drain reservoir within short period of time	X	X	X	
Emergency spillway located on embankment dam	X	X	X	X
Emergency spillway discharge encroaches on dam	X	X	X	X
Downstream valve control in an embankment dam		X	X	
OTHER	X	X	X	X

RANKING OF DAMS SCORING SUMMARY WORK SHEET

(Use Basic Information Summary Worksheet and Category Scoring Descriptions for each Category)

am Name		ID no.	Date	Engineer	
Section I. CON	SEQUENCES OF I	AILURE			
Category I.	Persons at Risk (P	AR) (For scoring se	e page 9):		
Zero PAR	1 – 3 PAR	4 – 30 PAR	31 – 300 PAR	> 300 PAR	Score
0 points	200 points	300 points	400 points	500 points	
Section II DO	TENTIAL FAILUR	E MODES AND SI	EDIOUGNIESS OF I	DEFICIENCIES	
ection II. PO	IENTIAL FAILUK	E MODES AND SI	EKIOUSNESS OF I	<u>DEFICIENCIES</u>	
Category II.A.	Hydrologic Adequ	acy (For scoring se	e page 10):		
Satisfactory	Minor	Moderate	Major	Severe	Score
0 points	20 points	65 points	145 points	300 points	
Category II.B.	Potential for Pipin				
Satisfactory	Minor	Moderate	Major	Severe	Score
			•		Score
0 points	20 points	65 points	145 points	300 points	Score
0 points Category II. C. Satisfactory	20 points Dam Stability (For	65 points scoring see pages Moderate	145 points 2 – 15): Major	300 points Severe	Score
0 points Category II. C.	20 points Dam Stability (For	65 points scoring see pages	145 points 2 – 15):	300 points	
0 points Category II. C. Satisfactory 0 points	20 points Dam Stability (For	65 points scoring see pages Moderate 65 points	145 points 2 – 15): Major 145 points	300 points Severe	
0 points Category II. C. Satisfactory 0 points	20 points Dam Stability (For Minor 20 points	Moderate 65 points Moderate 65 points or scoring see page Moderate	145 points 2 – 15): Major 145 points 16): Major	Severe 300 points Severe	
0 points Category II. C. Satisfactory 0 points Category II. D.	20 points Dam Stability (For Minor 20 points Outlet Conduit (For Minor 20 points)	65 points scoring see pages Moderate 65 points or scoring see page	145 points 2 – 15): Major 145 points 16):	300 points Severe 300 points	Score
0 points Category II. C. Satisfactory 0 points Category II. D. Satisfactory 0 points	20 points Dam Stability (For Minor 20 points Outlet Conduit (For Minor	Moderate 65 points Scoring see pages Moderate 65 points Moderate 65 points	145 points 2 – 15): Major 145 points 16): Major 145 points	Severe 300 points Severe	Score
0 points Category II. C. Satisfactory 0 points Category II. D. Satisfactory 0 points Category II. E.	20 points Dam Stability (For Minor 20 points Outlet Conduit (For Minor 20 points Unique Conditions	65 points Scoring see pages Moderate 65 points Or scoring see page Moderate 65 points S (For scoring see page)	145 points 2 – 15): Major 145 points 16): Major 145 points 16):	Severe 300 points Severe 300 points	Score
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0 points Category II. C. Satisfactory 0 points Category II. D. Satisfactory 0 points Category II. E. Satisfactory 0 points	20 points Dam Stability (For Minor 20 points) Outlet Conduit (For Minor 20 points) Unique Conditions Minor 20 points	Moderate 65 points Sor scoring see pages Moderate 65 points Moderate 65 points Grace For scoring see page Moderate 65 points Moderate 65 points	145 points 2 – 15): Major 145 points 16): Major 145 points Major 145 points Major 145 points	Severe 300 points Severe 300 points Severe 300 points	Score